



# **High Temperature Sulfidation of Carbon Steel under Claus Waste Heat Boiler Conditions**

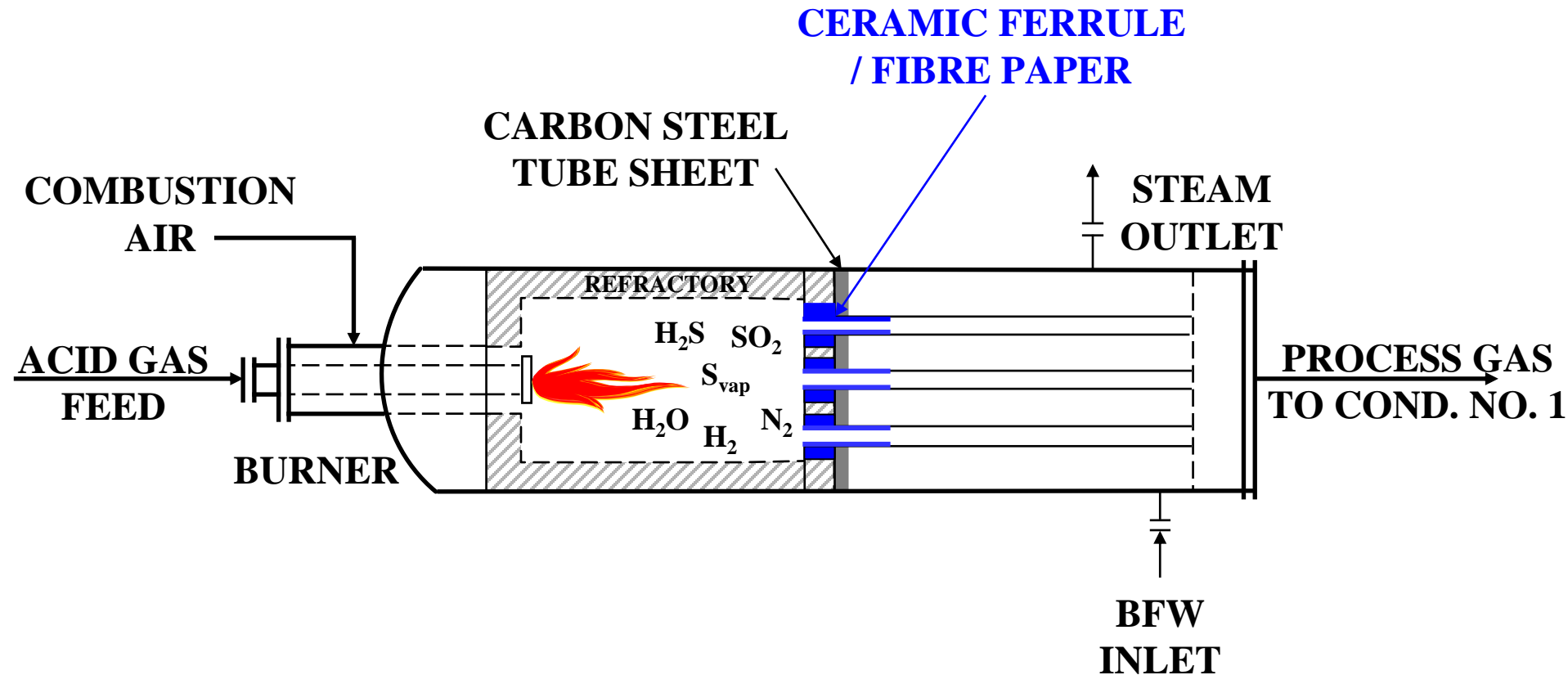
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# Overview of Claus Thermal Reactor and Waste Heat Boiler



- Ceramic ferrule / fibre paper thermal protection system for the critical tube-to-tube sheet area
- Current guide for  $T_{\max}$  design based on published correlations for high temperature sulfidic corrosion

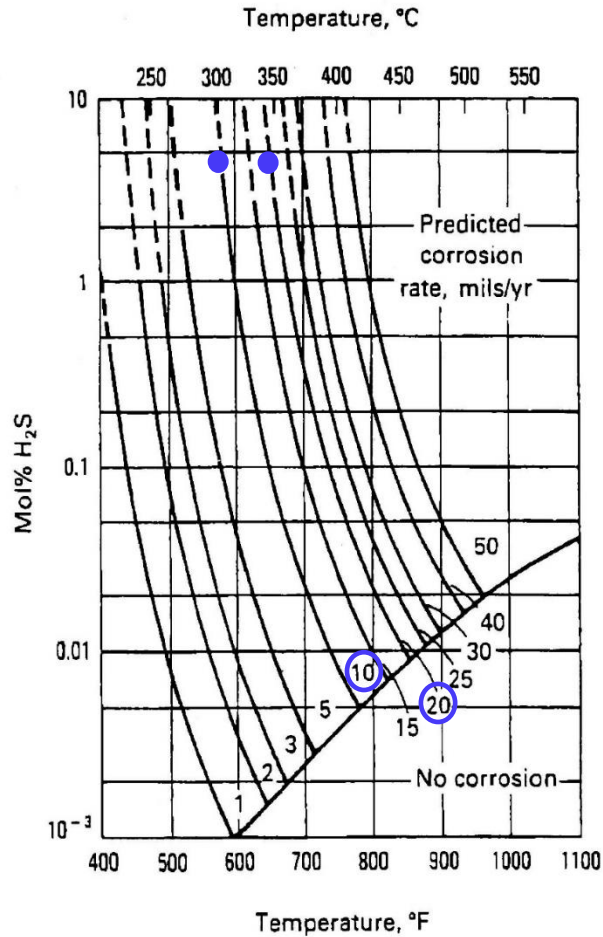


# High Temperature Sulfidic Corrosion of Carbon Steel

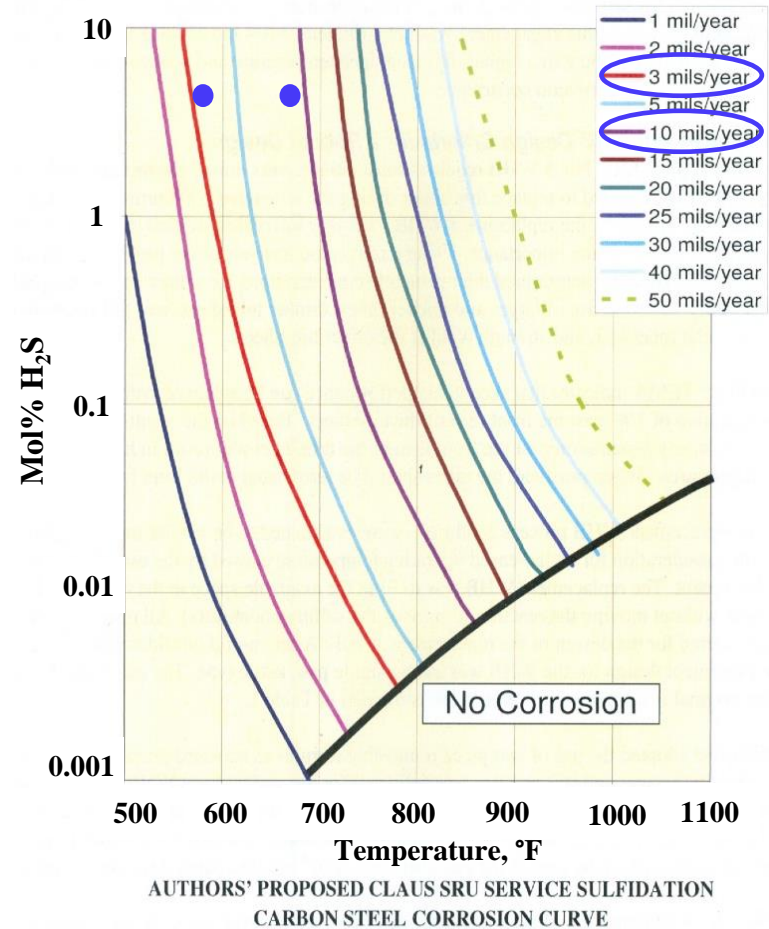
- **McConomy Curves**
  - Based on survey conducted by API Sub-committee on Corrosion (published 1963)
  - For high temperature sulfidic corrosion in  $H_2$ -free environment
  - Curves decreased by a factor of 2.5 in mid-1980's
  - Perhaps most useful for metallurgy selection
- **Couper-Gorman Curves**
  - Based on survey conducted by NACE Technical Committee T-8 on Refining Industry Corrosion (published 1971)
  - High temperature sulfidic corrosion in the presence of  $H_2$
  - Naphtha and gas / oil curves
  - Used as design basis for Claus WHB tube / tube sheet corrosion
- **Claus-modified Couper-Gorman Curves**
  - Curves shifted to predict lower corrosion rates in Claus SRU service
  - Based on operational experience



# Couper-Gorman (Naphtha) and Claus Modified Couper-Gorman Curves

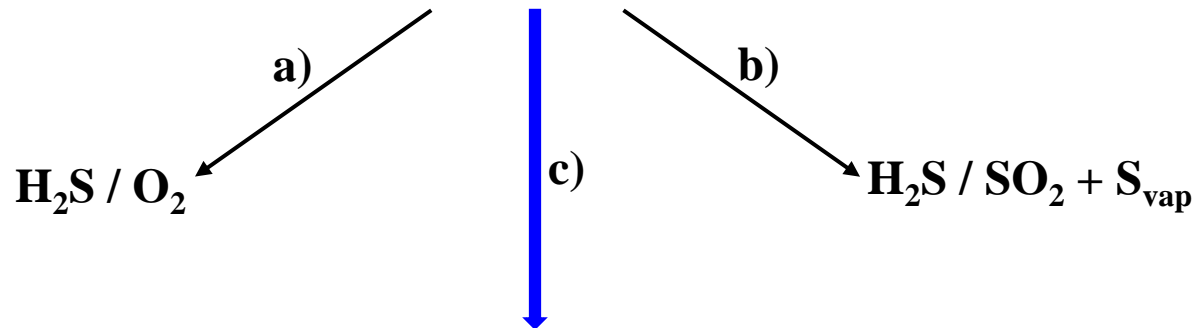


*Curves  
Shifted  
(100°F)*

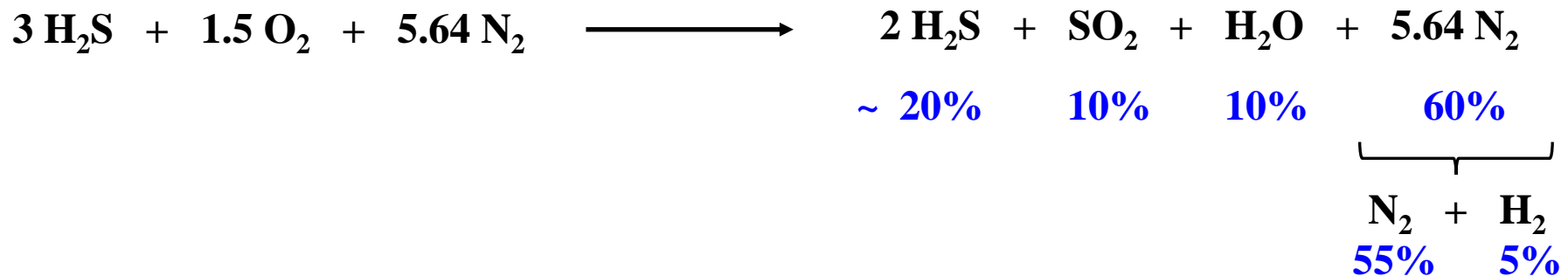




## Possible Approaches



*Use feed corresponding to post- $\text{H}_2\text{S}$  combustion / pre-Claus reaction and rely on Claus reaction to form elemental sulfur:*



- Need to add  $\text{H}_2$  to simulate WHB conditions in the lab experiments



## Experimental Conditions

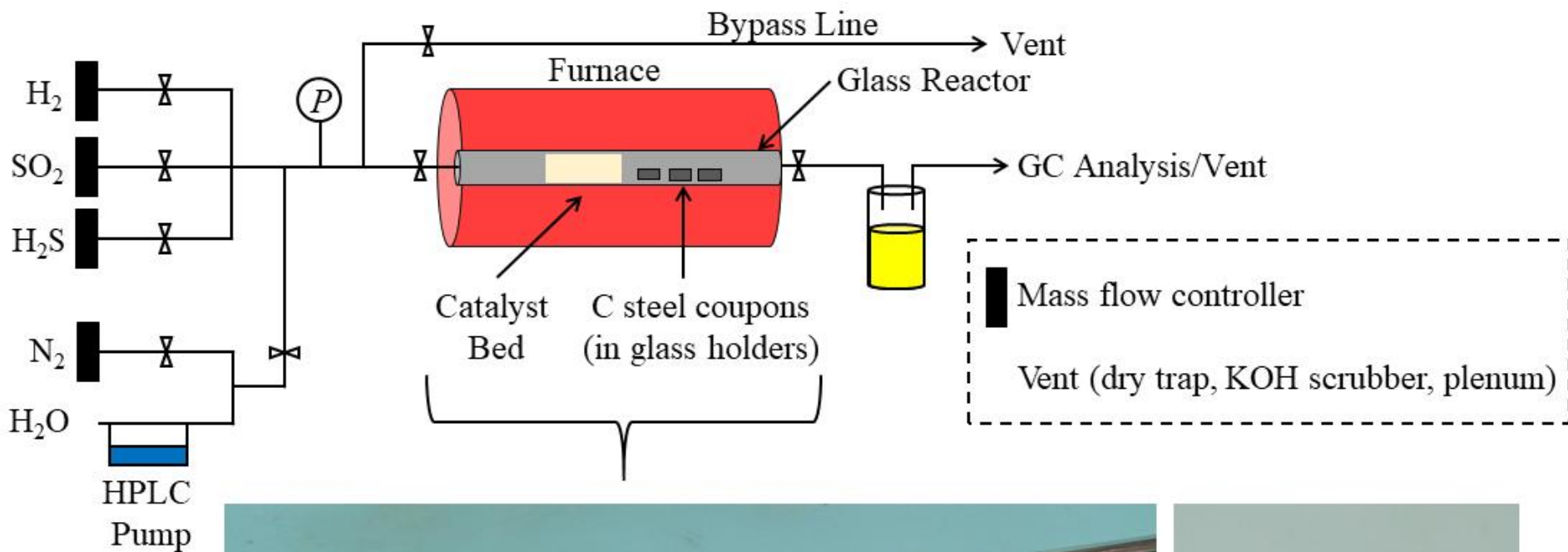
Temp. °C	H <sub>2</sub> S / SO <sub>2</sub> mol%	S <sub>2</sub> -S <sub>8</sub> mol%	N <sub>2</sub> mol%	H <sub>2</sub> mol%	H <sub>2</sub> O mol%
300	2 / 1	3.9	58.5	5	29.6
325	2.8 / 1.4	3.8	58.2	5	28.8
350	3.6 / 1.8	3.8	57.9	5	27.9
375	4.4 / 2.2	3.8	57.6	5	27.0
400	5.2 / 2.5	3.8	57.5	5	26.0

- Equilibrium furnace calculation gives *ca.* 5% H<sub>2</sub> (100% H<sub>2</sub>S / air)
- Carbon steel coupons; experimental temperatures of 300, 325, 350, 375, and 400°C
- Calculated liquid sulfur dew-point: 280°C
- Weight loss corrosion rates;  $W$  (g),  $D$  (g/cm<sup>3</sup>),  $A$  (cm<sup>2</sup>),  $t$  (h)

$$\text{Corrosion Rate (mpy)} = (3.45 \times 10^6 \times W) / (D \times A \times t)$$

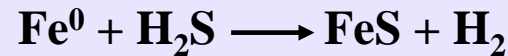
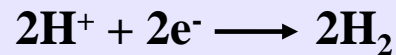
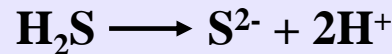


# Simplified Schematic of Experimental Setup





# High Temperature Sulfidic Corrosion

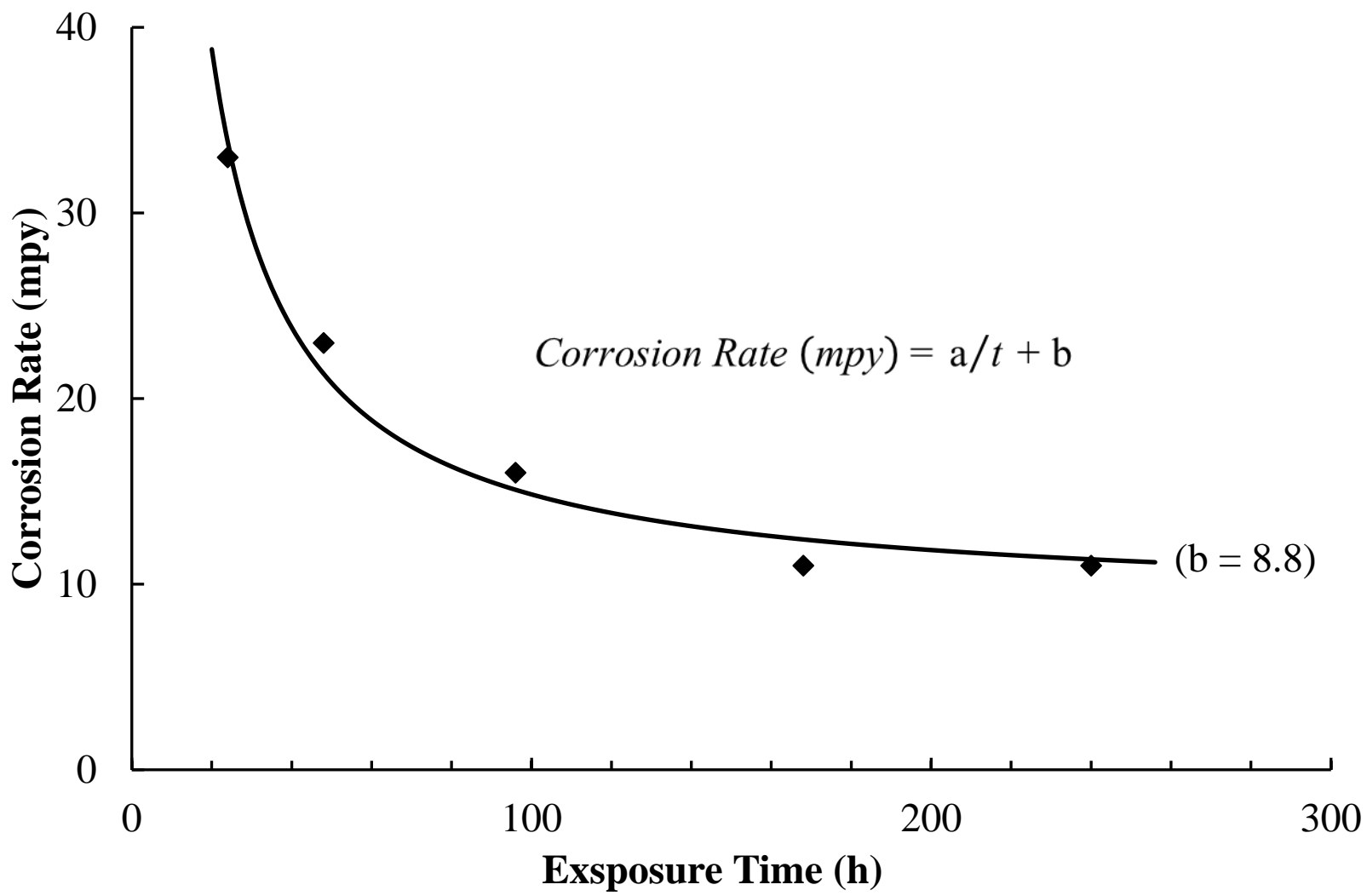


- **Nature and Stoichiometry of FeS**
  - Temperature,  $\text{H}_2\text{S}$  concentration, presence of other sulfur species, turbulence / erosion issues
  - Type of steel, heat treatment, Cr content, Si content, Mo content
- **$\text{Fe}_x\text{S}_y$  Semi-Protective Layer**
  - Limits the rate of diffusion of corrosive species
  - Ongoing sulfidation is limited by sulfur diffusion through the FeS film which is increasing in thickness
  - Initial period of rapid corrosion followed by a more gradual decrease and eventual stabilization in rate



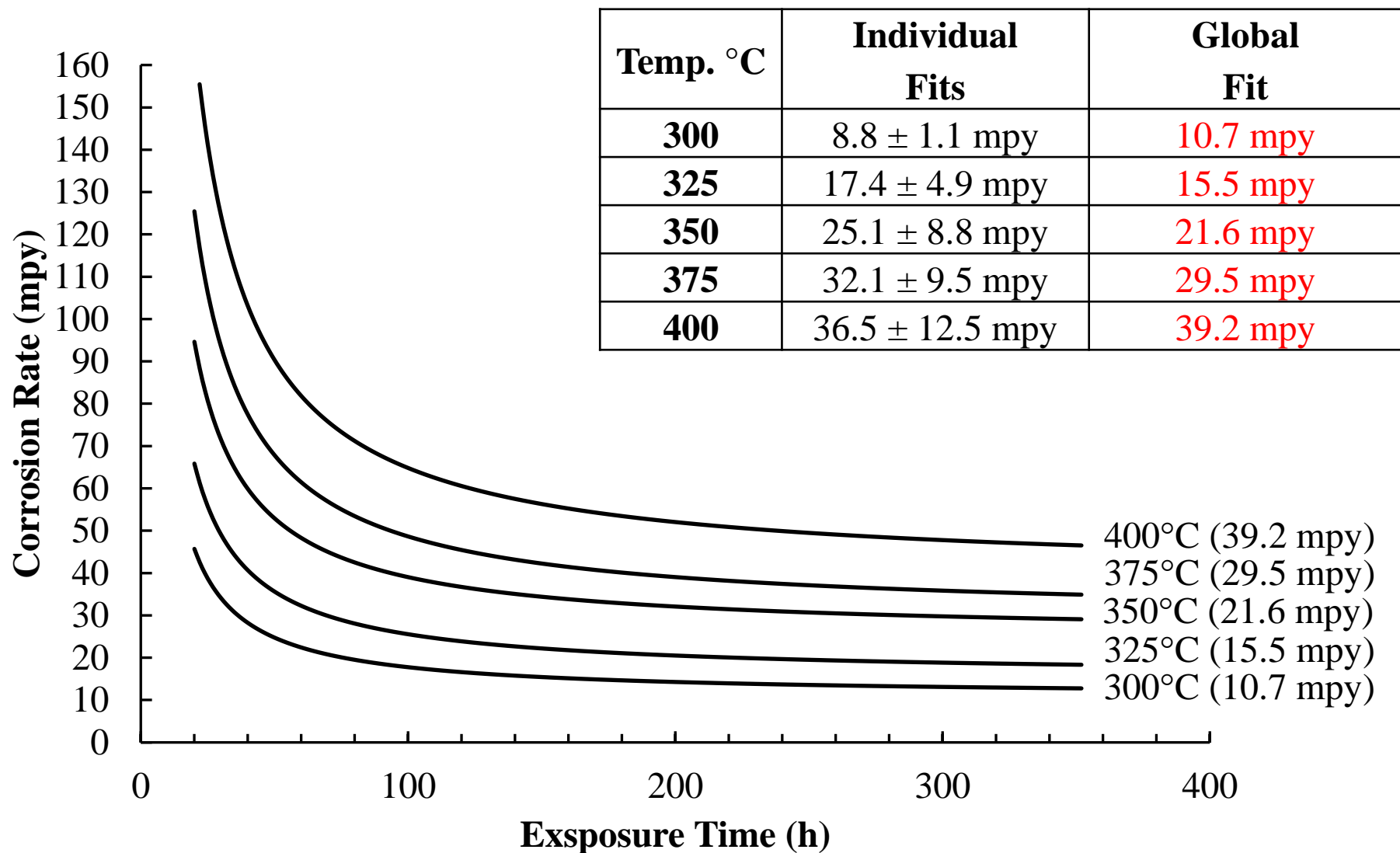


# Corrosion Profile at 300°C





# Corrosion Profiles using Global Expression; H<sub>2</sub>S (2-5 mol%)





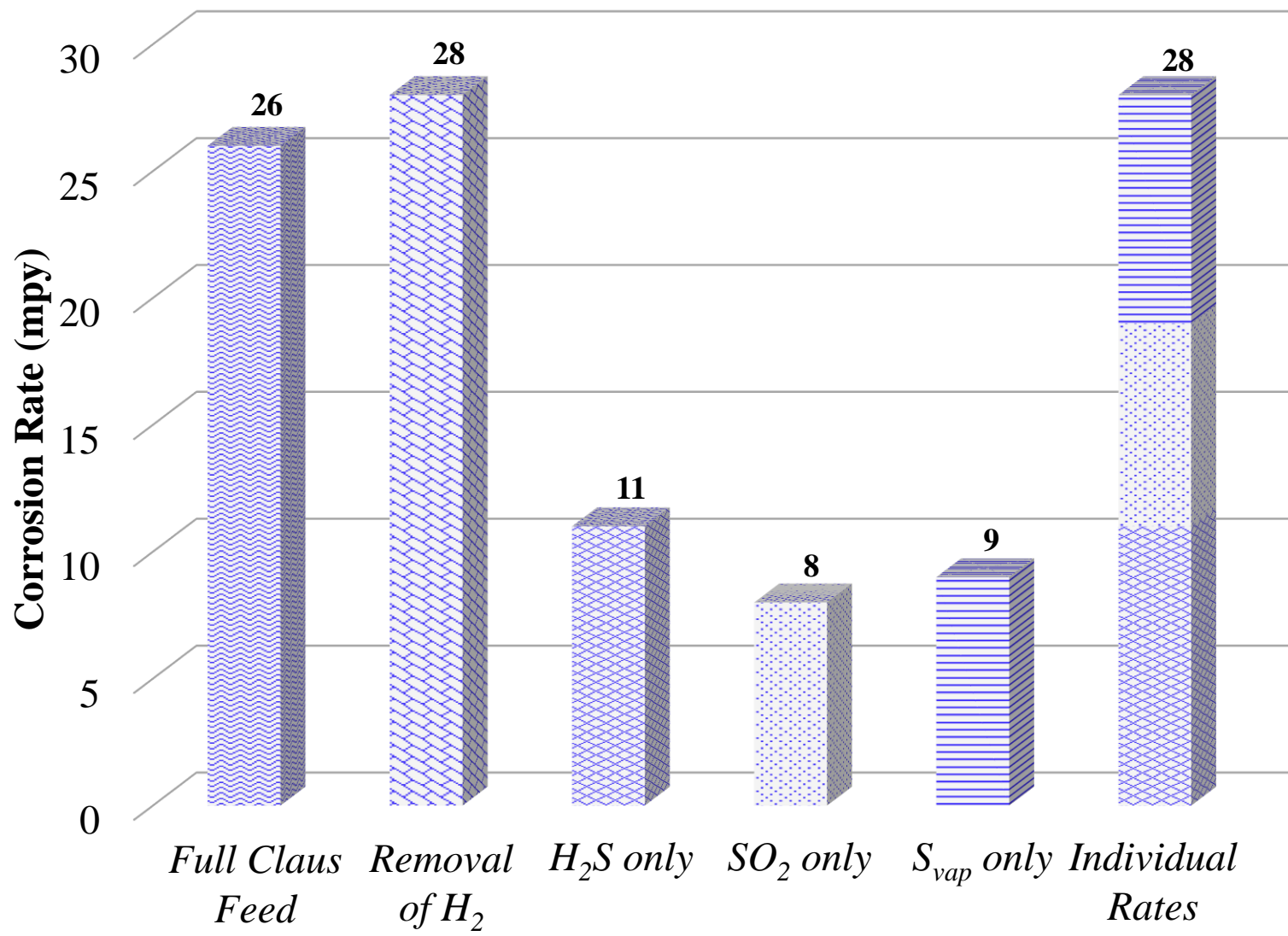
# Comparison to Existing Correlations at Corresponding $T$ and $H_2S$ Concentration

Temp. °C	Corr. Rate (mpy) This work	Corr. Rate (mpy) Couper-Gorman <sup>a</sup>	Corr. Rate (mpy) Couper-Gorman <sup>b</sup>	Corr. Rate (mpy) Martens et. al.
300	11	<i>ca. 7</i>	<i>ca. 15</i>	<i>ca. 3</i>
325	16	<i>ca. 15</i>	<i>ca. 20</i>	<i>ca. 5</i>
350	22	<i>ca. 20</i>	<i>ca. 40</i>	<i>ca. 8</i>
375	30	<i>ca. 30</i>	<i>ca. 60</i>	<i>ca. 13</i>
400	39	<i>ca. 45</i>	<i>ca. 80</i>	<i>ca. 20</i>

<sup>a</sup>Naphtha desulfurizers, <sup>b</sup>Gas / Oil desulfurizers

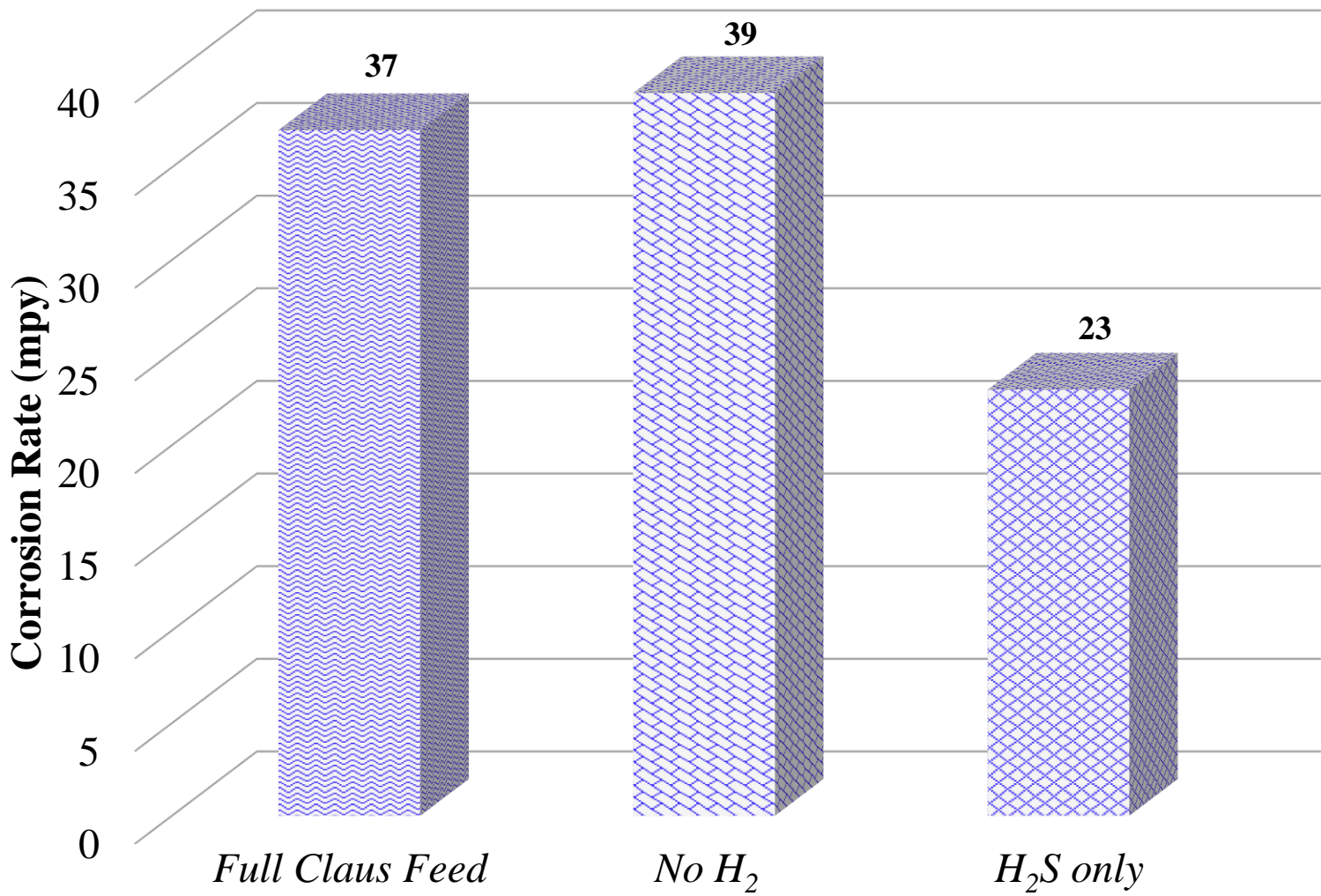


# Stabilized Corrosion Rates Measured at 350°C



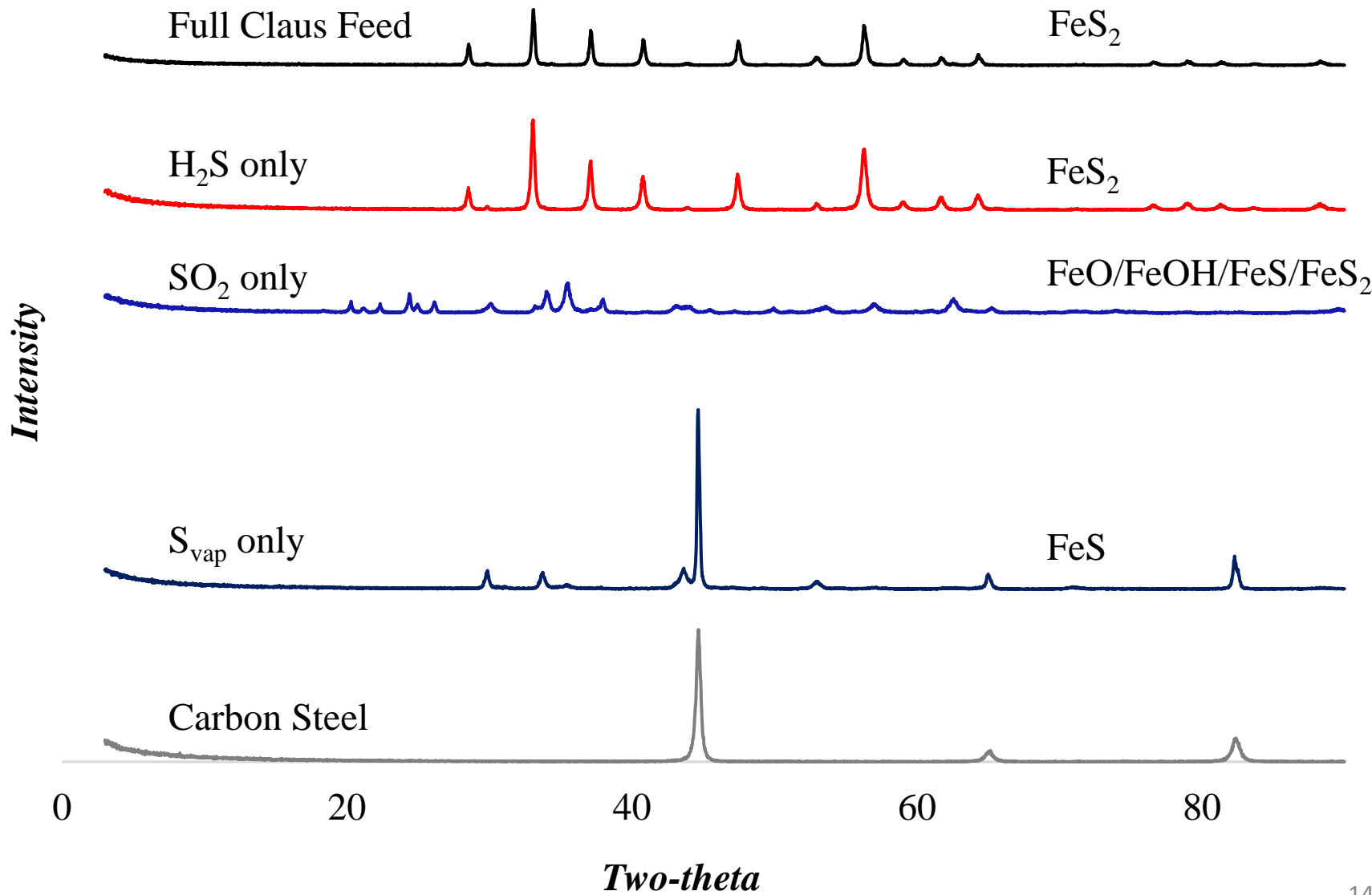


# Stabilized Corrosion Rates Measured at 400°C



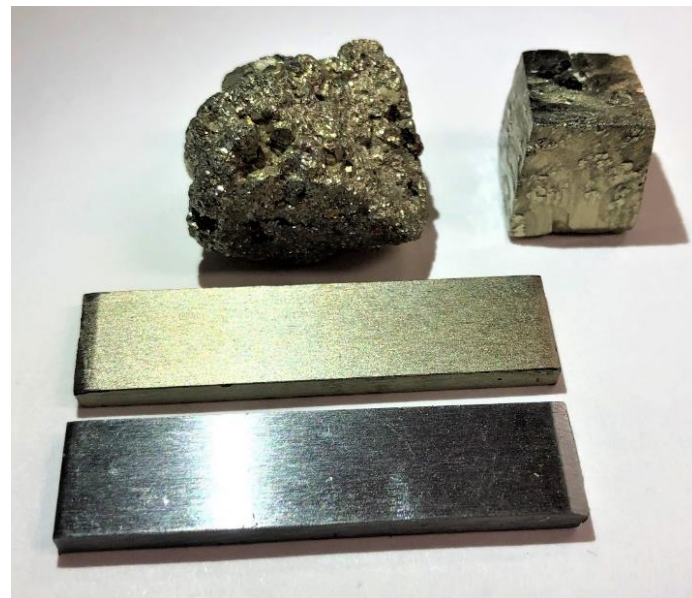


# XRD Analysis of Various Corrosion Scales





- **Global Expression**
  - Most accurate for conditions ( $\text{H}_2\text{S}$  2-5 mol%) similar to those employed in this study
- **Results match best with naphtha Couper-Gorman curves**
  - Most likely just serendipitous
  - Presence/absence of 5 mol%  $\text{H}_2$  did not influence corrosion rates significantly
- **Corrosion Scale Formed ( $\text{FeS}_2$ )**
  - $\text{H}_2\text{S}$ ,  $\text{SO}_2$ , and  $\text{S}_{\text{vap}}$  all contribute to overall corrosion rate
  - $\text{H}_2\text{S}$  plays key role in formation of pyrite ( $\text{FeS}_2$ )
- **Recommend Lowest Temperature Practically Possible**
  - In agreement with recent recommendation of  $\leq 315^\circ\text{C}$
- **Need to Investigate other Scenarios**
  - More varied  $\text{H}_2\text{S}$  concentrations ( $\text{O}_2$  enrichment)
  - Impact of  $\text{NH}_3$
  - Other alloys







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